



**Autonomous Vehicle Simulation (AVS) Laboratory,  
University of Colorado**

**Basilisk Technical Memorandum  
Document ID: Basilisk-attTrackingError  
ATTITUDE TRACKING ERROR**

Prepared by	H. Schaub
-------------	-----------

<b>Status:</b> Reviewed
<b>Scope/Contents</b>
This module is intended to be the last module in the guidance module chain. It's input is the reference motion message generated by a prior module. It's output is at the guidance attitude tracking errors relative to a moving reference frame. This module applies the body to corrected body attitude correction.

Rev	Change Description	By	Date
1.0	First Verision	H. Schaub	2016-01-15
1.1	Revision and reformatting	T. Teil	2019-02-20

## Contents

<b>1</b>	<b>Model Description</b>	<b>1</b>
1.1	Introduction . . . . .	1
1.2	Reference Frame Definitions . . . . .	1
1.3	Reference Frame Angular Velocity Vector . . . . .	2
1.4	Reference Frame Angular Acceleration Vector . . . . .	3
1.5	Angular Velocity Tracking Error . . . . .	3
<b>2</b>	<b>Module Functions</b>	<b>3</b>
<b>3</b>	<b>Module Assumptions and Limitations</b>	<b>3</b>
<b>4</b>	<b>Test Description and Success Criteria</b>	<b>3</b>
<b>5</b>	<b>Test Parameters</b>	<b>3</b>
<b>6</b>	<b>Test Results</b>	<b>4</b>
<b>7</b>	<b>User Guide</b>	<b>4</b>

---

## 1 Model Description

### 1.1 Introduction

This technical note outlines how the attitude tracking errors are evaluated relative to a given reference frame. The reference frame from the chain of guidance modules is called  $\mathcal{R}_0$ , while the body corrected reference frame orientation is  $\mathcal{R}$ .

### 1.2 Reference Frame Definitions

Let the primary body-fixed coordinate frame be  $\mathcal{B} : \{\hat{\mathbf{b}}_1, \hat{\mathbf{b}}_2, \hat{\mathbf{b}}_3\}$ . However, instead of aligning this frame with a reference, a corrected body frame  $\mathcal{B}_c$  is to be aligned with a reference frame. Let the uncorrected reference orientation be given by  $\mathcal{R}_0$ . Thus, the guidance goal is to drive  $\mathcal{B}_c \rightarrow \mathcal{R}_0$ , which yields

$$[R_0N] = [B_cB][BN] \quad (1)$$

where  $\mathcal{N}$  is an inertial reference frame. Rearranging this relationship, with perfect attitude tracking the inertial body frame orientation should be

$$[BN] = [B_cB]^T[R_0N] = [RN] \quad (2)$$

where  $\mathcal{R}$  is a corrected reference frame. Note that  $[B_cB] = [R_0R]$ . Thus, the corrected reference orientation is computed using

$$[RN] = [R_0R]^T[R_0N] \quad (3)$$

where the body-frame correction is subtracted from the original reference orientation.

The benefit of driving  $\mathcal{B} \rightarrow \mathcal{R}$  instead of  $\mathcal{B}_c \rightarrow \mathcal{R}_0$  is that the body frame, along with the many device position and orientation vectors expressed in body-frame components, don't have to be rotated for each control evaluation. In simple terms, if the corrected body frame is a  $60^\circ$  rotation from the body

frame, then the  $60^\circ$  is subtracted from the original reference orientation. This allows all body inertia tensor and reaction wheel heading vector descriptions to remain in the primary body frame  $\mathcal{B}$ .

Assume the initial uncorrected reference frame  $\mathcal{R}_0$  is given through the MRP set  $\sigma_{R_0/N}$

$$[R_0N(\sigma_{R_0/N})] \quad (4)$$

The relative orientation of the corrected body frame relative to the primary body frame is a constant MRP set

$$[B_cB(\sigma_{B_c/B})] = [R_0R(\sigma_{R_0/R})] \quad (5)$$

To apply this correction to the original reference frame, using the Direction Cosine Matrix (DCM) description, this is determined through

$$[RN(\sigma_{R/N})] = [R_0R(\sigma_{R_0/R})]^T [R_0N(\sigma_{R_0/N})] = [R_0R(-\sigma_{R_0/R})][R_0N(\sigma_{R_0/N})] \quad (6)$$

where the convenient MRP identity

$$[R_0R(\sigma_{R_0/R})]^T = [R_0R(-\sigma_{R_0/R})] \quad (7)$$

Note the following MRP addition property developed in Reference ?. If

$$[BN(\sigma)] = [FB(\sigma'')][BN(\sigma')] \quad (8)$$

then

$$\sigma = \frac{(1 - |\sigma'|^2)\sigma'' + (1 - |\sigma''|^2)\sigma' - 2\sigma'' \times \sigma'}{1 + |\sigma'|^2|\sigma''|^2 - 2\sigma' \cdot \sigma''} \quad (9)$$

In the RigidBodyKinematics software library of Reference ?, this MRP evaluation is achieved with

$$\sigma = \text{addMRP}(\sigma', \sigma'')$$

Thus, to properly apply the body frame orientation correction to the original reference frame, this function should be used with

$$\sigma_{R/N} = \text{addMRP}(\sigma_{R_0/N}, -\sigma_{R_0/R})$$

The attitude tracking error of  $\mathcal{B}$  relative to  $\mathcal{R}$  is

$$\sigma_{B/R} = \text{subMRP}(\sigma_{B/N}, -\sigma_{R/N})$$

### 1.3 Reference Frame Angular Velocity Vector

The angular velocity of the original reference frame  $\mathcal{R}_0$  is

$$\omega_{R_0/N} \quad (10)$$

The angular velocity tracking error is defined as

$$\delta\omega = \omega_{B/N} - \omega_{R/N} \quad (11)$$

The correct reference frame angular velocity is

$$\omega_{R/N} = \omega_{R/R_0} + \omega_{R_0/N} = \omega_{R_0/N} \quad (12)$$

because the body frame correction  $[B_cB] = [R_0R]$  is a constant angular offset.

The required inertial reference frame rate vector, in body frame components, is then given by

$${}^{\mathcal{B}}\omega_{R/N} = [BN]^{\mathcal{N}}\omega_{R/N} \quad (13)$$

## 1.4 Reference Frame Angular Acceleration Vector

With  $\dot{\omega}_{R/N}$  given in the inertial frame, in the body frame this vector is expressed as

$${}^{\mathcal{B}}\dot{\omega}_{R/N} = [BN]{}^{\mathcal{N}}\dot{\omega}_{R/N} \quad (14)$$

## 1.5 Angular Velocity Tracking Error

Finally, the angular velocity tracking error is expressed in body frame components as

$${}^{\mathcal{B}}\delta\omega = {}^{\mathcal{B}}\omega_{B/R} = {}^{\mathcal{B}}\omega_{B/N} - {}^{\mathcal{B}}\omega_{R/N} \quad (15)$$

## 2 Module Functions

The only specific function to this module is the error computation function. It's only goal is to remove the computation from the update function itself.

- **computeAttitudeError**: This function calculates computes the attitude error between the reference and the spacecraft attitude.

## 3 Module Assumptions and Limitations

No assumptions or limitations are made specifically in this module. It simply uses the input messages to output an error between two different attitudes and rates.

## 4 Test Description and Success Criteria

The unit test instantiates the module and writes out a reference attitude message as well as a spacecraft navigation message. It then compares the module outputs to expected results.

## 5 Test Parameters

In order to test the proper implementation of this module, the unit test verify that the module output guidance message vectors match expected values.

**Table 2:** Error tolerance for each test.

Output Value Tested	Tolerated Error
$\sigma_{BR}$	$10^{-12}$
${}^{\mathcal{B}}\omega_{BR}$	$10^{-12}$
${}^{\mathcal{B}}\omega_{RN}$	$10^{-12}$
${}^{\mathcal{B}}\delta\omega_{RN}$	$10^{-12}$

The error tolerances are given in Table 2, while initial conditions used in this test are as follows:

**Table 3:** Initial conditions

Navigation Information	Value
$\sigma_{BN}$	$[0.25 \quad -0.45 \quad 0.75]^T$
${}^{\mathcal{B}}\omega_{BN}$	$[0.25 \quad -0.45 \quad 0.75]^T$
Reference Information	Value
$\sigma_{RN}$	$[0.35 \quad -0.25 \quad 0.15]^T$
${}^{\mathcal{N}}\omega_{RN}$	$[0.018 \quad -0.032 \quad 0.015]^T$
$\delta{}^{\mathcal{N}}\omega_{RN}$	$[0.048 \quad -0.022 \quad 0.025]^T$

Finally the precomputed expected values for the test are give in the following table:

**Table 4:** Precomputed Expected values

Output Value Tested	Tolerated Error
$\sigma_{BR}$	$[0.1836841481753408 \quad -0.0974447769418166 \quad -0.09896069560518146]^T$
${}^B\omega_{BR}$	$[-0.01181207648013235 \quad -0.008916032420030655 \quad -0.0344122606253076]^T$
${}^B\omega_{RN}$	$[-0.003187923519867655 \quad -0.003083967579969345 \quad 0.0394122606253076]^T$
${}^B\delta\omega_{RN}$	$[-0.02388623421245188 \quad -0.02835600277714878 \quad 0.04514847640452802]^T$

## 6 Test Results

All of the tests passed:

**Table 5:** Test results

Check	Pass/Fail
1	PASSED
2	PASSED
3	PASSED
4	PASSED

## 7 User Guide

The user only needs to setup the module and link the proper message names:

- Build the C-struct:
 

```
moduleConfig = attTrackingError.attTrackingErrorConfig()
```
- Wrap the module:
 

```
moduleWrap = alg_contain.AlgContain(moduleConfig,
attTrackingError.Update_attTrackingError,
attTrackingError.SelfInit_attTrackingError,
attTrackingError.CrossInit_attTrackingError)
moduleWrap.ModelTag = "attTrackingError"
```
- Add the module to the task:
 

```
unitTestSim.AddModelToTask(unitTaskName, moduleWrap, moduleConfig)
```
- Link message names. For instance:
 

```
moduleConfig.inputNavName = "inputNavName"
moduleConfig.inputRefName = "inputRefName"
moduleConfig.outputDataName = "outputName"
```
- Set the R0R vector:
 

```
moduleConfig.sigma_R0R = [0.01, 0.05, -0.55]
```