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## ORTHOGONAL SQUARE ROOT EIGENFACTOR PARAMETERIZATION OF MASS MATRICES\*

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An improved method is presented to parameterize a smoothly time varying symmetric, positive definite system mass matrix M(t) in terms of the instantaneous eigenfactors, namely the eigenvalues and eigenvectors of M(t). Differential equations are desired whose solution generate the instantaneous spectral decomposition of M(t). The derivation makes use of the fact that the eigenvector matrix is orthogonal and thus evolves analogously to a higher dimensional rotation matrix. Careful attention is given to cases where some eigenvalues and/or their derivatives are equal or near-equal. A robust method is presented to approximate the corresponding eigenvector derivatives in these cases which ensures that the resulting eigenvectors still diagonalize the instantaneous M(t) matrix. This method is also capable of handling the rare case of discontinuous eigenvectors which may only occur if both the corresponding eigenvalues and their derivatives are equal.

#### I. Introduction

MOST multibody dynamical systems such as multi-link robots have configuration dependent mass matrices. This dependency makes the mass matrix vary with time. Solving such dynamical systems involves performing an inverse of the mass matrix at each integration step. Finding this inverse is computationally difficult and expensive for large systems. Furthermore, standard inverse and linear equations solution techniques are not easily parallelizable and therefore cannot take full advantage of modern parallel computing systems.

A method is introduced that parameterizes the symmetric, positive definite mass matrix in terms of its eigenfactors (i.e. eigenvectors and the eigenvalues). Instead of forward integrating the original mass matrix differential equation directly, only the eigenfactors themselves are forward integrated. The resulting formulation is one that could be easily implemented on a massively parallel computer system. A paper by Oshman and Bar-Itzhack in Ref. 1 introduces an orthogonal square root eigenfactor parameterization to solve the differential matrix Riccati equation. However, their treatment of equal or near-equal eigenvalues was found to be incorrect and the case of discontinuous eigenvectors was not accounted for. This paper provides an approximate

treatment of the near-equal eigenvalue case and an associated error analysis where the symmetric, positive definite matrix being parameterized is a state dependent mass matrix M(x,t).

Eigenfactor derivatives have been discussed in the literature for quite some time, but they are mostly used to establish modal sensitivities and not to derive eigenfactor differential equations.<sup>2,3</sup> A majority of the engineering literature on eigenfactor derivatives are for the general structural eigenvalue problem  $(K - \lambda_i M)v_i = 0$ . This paper deals with the problem where we need to find the eigenfactors and their derivatives for given matrices M(x,t) and M(x,x,t). Since M is symmetric and positive definite, its eigenvector matrix is guaranteed to be orthogonal and thus behave analogously to a higher dimensional rotation direction cosine matrix.<sup>4,5</sup> This analogy is the starting point for a simple derivation of the eigenfactor derivatives. Except for repeated eigenvalues, for smooth M(x,t), we anticipate continuous differentiable eigenfactors.

When repeated eigenvalues are present there are often numerical problems associated with calculating the eigenvector derivatives. The literature usually deals with the case where M and  $\dot{M}$  are given and one needs to solve for the eigenfactor derivatives.  $^{6-9}$  A simple method is presented which allows the eigenvectors to be smoothly integrated through the case of repeated eigenvalues, avoiding having to re-solve an algebraic eigenvector, eigenvalue problem

Repeated eigenvalues for mass matrices are common in mechanics (e.g. principal axes for mass

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matrices and stress tensors). We note that, if the objective is to find a diagonalizing transformation, then near-repeated eigenvalues only indicate a loss of uniqueness of the eigenvectors. For many purposes uniqueness is not required, and any set of orthogonal eigenvectors which span a unique subspace are admissible. This is the approach realized in the present paper when eigenvectors loose their uniqueness for near-repeated eigenvalues; we seek to generate admissible orthogonal eigenvectors which span the correct subspace to within acceptable precision. This line of thinking is easily implemented for solving the algebraic eigenvalue problem for a given constant matrix — however, generating the time varying instantaneous eigensolution by solving differential equations governing the eigenfactors is a more challenging task that is addressed in this paper.

#### II. Problem Statement

Any real, symmetric, positive definite matrix M of dimension  $n \times n$  can be decomposed into n positive real eigenvalues  $\lambda_i$  and n orthogonal eigenvectors  $c_i$ 

$$M = C^T \Lambda C \tag{1}$$

where  $\Lambda = diag(\lambda_i)$  and C is is defined as

$$C = \left[c_1 \cdots c_n\right]^T \tag{2}$$

The evolution of the C eigenvector matrix is completely analogous to the time variation of an orthogonal direction cosine attitude matrix. Since M is symmetric and positive definite, the eigenvector matrix C is guaranteed to be orthogonal

$$C^T C = C C^T = I \tag{3}$$

and the eigenvalues will always be positive. Thus we can always define  $s_i = \sqrt{\lambda_i}$  and the corresponding matrix  $S = diag(s_i)$ . This allows M to be written as

$$M = C^T S^T S C = W^T W \tag{4}$$

where W = SC is a matrix square root of M. Therefore keeping track of C and S is equivalent to a square root algorithm with all the associated numerical robustness advantages.<sup>1</sup> Note that since  $s_i, \lambda_i > 0$ , the matrix inverse of M is trivial.

$$M^{-1} = C^T S^{-2} C (5)$$

Let x be a continuous system state vector satisfying the second order dynamical differential equation

$$M(x)\ddot{x} = F(x, \dot{x}, u) \tag{6}$$

where u is a control vector. Any discontinuity in u can only directly affect  $\ddot{x}$  and not  $\dot{x}$  or x. Therefore

the matrices M(x) and  $\dot{M}(x,\dot{x},t)$  are continuous. Note that complete algebraic expressions for M(x) and  $\dot{M}(x,\dot{x},t)$  are usually available for dynamical systems.

#### III. Eigenfactor Derivatives

The fact that the eigenvector matrix C that parameterize a symmetric, positive definite matrix M is always orthogonal will be central in the following derivation of the eigenfactor derivatives. It is known that an  $n \times n$  orthogonal matrix C(t) satisfies the same differential equation as does the attitude direction cosine matrix<sup>5,10</sup>

$$\dot{C} = -[\Omega]C \tag{7}$$

where  $[\Omega]$  is a skew-symmetric matrix.

$$[\Omega] = \begin{bmatrix} 0 & \Omega_{12} & \Omega_{13} \\ -\Omega_{12} & 0 & \Omega_{23} \\ -\Omega_{13} & -\Omega_{23} & 0 \end{bmatrix}$$
(8)

For the case of attitude matrices, this  $\Omega_{ij}$  terms represent body angular velocities. This concept of angular velocities lifts to the case of higher dimensional orthogonal matrices. Instead of being body angular velocities, here the  $\Omega_{ij}$  terms can be viewed as eigenvector angular velocities. Each  $\Omega_{ij}$  term gives a measure of the rate that the two eigenvectors  $c_i$  and  $c_j$  are rotating in the plane spanned by these two vectors.

To verify that orthogonal matrices are indeed generated by the given differential equation, the first derivative of Eq. (3) is taken

$$\dot{C}^T C + C^T \dot{C} = \dot{C} C^T + C \dot{C}^T = 0 \tag{9}$$

After substituting  $\dot{C}$  with Eq. (7)

$$-C^{T}[\Omega]^{T}C - C^{T}[\Omega]C = -[\Omega]CC^{T} - CC^{T}[\Omega]^{T} = 0$$
(10)

and making use of the orthogonality condition in Eq. (3) and the fact that  $[\Omega] = -[\Omega]^T$ , the differential equation for orthogonal matrices in Eq. (7) is verified.

The problem of finding eigenvector derivatives has now been reduced to one of finding the  $\Omega_{ij}$  terms. Taking the first derivative of Eq. (1) we obtain

$$\dot{M} = C^T \Lambda \dot{C} + \dot{C}^T \Lambda C + C^T \dot{\Lambda} C \tag{11}$$

After making use of Eq. (7) and defining the symmetric  $\xi$  matrix to be

$$\xi = \Lambda[\Omega] - [\Omega]\Lambda \tag{12}$$

Eq. (11) is reduced to

$$\dot{M} = C^T(\xi + \dot{\Lambda})C \tag{13}$$

The  $\xi$  matrix can be shown to be

$$\xi_{ij} = \Omega_{ij}(\lambda_j - \lambda_i) \tag{14}$$

Note that since the diagonal terms of  $\xi$  are zero and  $\dot{\Lambda}$  is a diagonal matrix, these two matrices projected through C split up the  $\dot{M}$  matrix into diagonal and off-diagonal terms. It turns out that the diagonal terms lead to the eigenvalue derivatives and the off-diagonal terms leads to the angular velocity terms. Let the matrix  $\mu$  be

$$\mu = C\dot{M}C^T \tag{15}$$

Using Eq. (14) this is rewritten as

$$\mu = \xi + \dot{\Lambda} \tag{16}$$

which can be component wise expressed as

$$\mu_{ij} = \begin{cases} \Omega_{ij}(\lambda_j - \lambda_i) & \text{for } i \neq j \\ \dot{\lambda}_i & \text{for } i = j \end{cases}$$
 (17)

Note that Eq. (17) must always hold, even in the presence of repeated eigenvalues. Also, as long as  $\Omega_{ij}$  is bounded, then  $\mu_{ij}$  must go to zero as  $\lambda_i \to \lambda_j$ . From here it is trivial to express  $\Omega_{ij}$  as<sup>1,2,4</sup>

$$\Omega_{ij} = \frac{\mu_{ij}}{\lambda_j - \lambda_i} \quad for \ \lambda_i \neq \lambda_j$$
 (18)

or in terms of the square roots of the eigenvalues as

$$\Omega_{ij} = \frac{\mu_{ij}}{s_j^2 - s_i^2} \quad for \ s_i \neq s_j$$
 (19)

At first glance it might appear that  $\Omega_{ij}$  will go to infinity when  $\lambda_i \to \lambda_j$ . However, this is generally not the case as will be shown in the next section.

Had an eigenvector matrix  $V = C^T$  been used instead to parameterize M in Eq. (1), then V would have also been orthogonal and abided by the same differential equation as in Eq. (7) with a different  $[\Omega]$  matrix.

$$\dot{V} = -[\bar{\Omega}]V \tag{20}$$

However, finding this  $[\bar{\Omega}]$  matrix is more difficult and can only be achieved through a coordinate transformation of the  $[\Omega]$  matrix

$$[\bar{\Omega}] = -V[\Omega]V^T \tag{21}$$

In rotational dynamics, this would be analogous to writing the body angular velocity matrix in the inertial frame. This is why the current development uses C instead of V.

Expressions for  $\lambda_i$  are found directly from Eq. (17)

$$\dot{\lambda}_i = \mu_{ii} = \Gamma_{ii} \tag{22}$$

where  $\Gamma = diag(\mu_{ii})$ . Since  $s_i = \sqrt{\lambda_i}$  the derivative of  $s_i$  is

$$\dot{s}_{i} = \frac{1}{2} \dot{\lambda}_{i} \lambda_{i}^{-\frac{1}{2}} = \frac{1}{2} \dot{\lambda}_{i} s_{i}^{-1}$$
 (23)

or in matrix  $form^{1,4}$ 

$$\dot{S} = \frac{1}{2}\Gamma S^{-1} \tag{24}$$

Note that calculating  $s_i^{-1}$  is always possible since for symmetric, positive definite matrices all eigenvalues are always positive.

Turns out the by far largest computational effort in evaluating C and S is finding the  $\mu_{ij} = c_i^T \dot{M} c_j$  terms. However, this inner product operation lends itself perfectly to be performed on a massively parallel computer system where all the  $\mu_{ij}$  terms could be calculated independently in parallel. By contrast direct matrix inverse method do not lend themselves easily to be calculated on parallel systems.

#### IV. Repeated Eigenvalues

#### A. Distinct Eigenvalue Derivatives

Clearly mathematical problems arise computing  $\Omega_{ij}$  using Eqs. (18) or (19) when  $\lambda_i \to \lambda_j$ . Whenever  $\lambda_i = \lambda_j$  the associated eigenvectors  $c_i$  and  $c_j$  that parameterize M are not unique. Any two orthogonal unit vectors in the plane spanned by  $c_i$  and  $c_j$  would generate the proper M matrix. However, the eigenfactors not only have to generate the proper M matrix, but they and their derivatives also need to generate the proper continuous M matrix. This leads to the following proposition about the continuity of  $c_i$  and  $c_j$  through the point where  $\lambda_i = \lambda_j$ .

Proposition 1: Let M be a continuous symmetric, positive definite matrix with a continuous derivative M and let  $\lambda_i$  and  $\lambda_j$  be repeated eigenvalues of M with distinct derivatives  $\lambda_i \neq \lambda_j$ . Then the associated eigenvectors will be continuous and unique through the condition where  $\lambda_i = \lambda_j$ .

*Proof:* To prove this proposition, let us write M as<sup>11</sup>

$$M = \sum_{i=1}^{n} \lambda_i E_i \tag{25}$$

where  $E_i$  is defined as the outer product

$$E_i = c_i c_i^T (26)$$

The matrix  $\dot{M}$  can now be written as

$$\dot{M} = \sum_{i=1}^{n} \left( \dot{\lambda}_i E_i + \lambda_i \dot{E}_i \right) \tag{27}$$

Without loss of generality, we can assume that only the first two eigenvalues  $\lambda_1$  and  $\lambda_2$  are repeated. Let us define  $E_{ij}$  as

$$E_{ij} = E_i + E_j \tag{28}$$

then we can rewrite  $\dot{M}$  as

$$\dot{M} = \dot{\lambda}_1 E_1 + \dot{\lambda}_2 E_2 + \lambda_1 \dot{E}_{12} + \sum_{i=3}^n \left( \dot{\lambda}_i E_i + \lambda_i \dot{E}_i \right) \tag{29}$$

Since  $\dot{M}$  must be continuous,  $c_1$  and  $c_2$  cannot be discontinuous since the eigenvalue derivatives  $\dot{\lambda}_1$  and  $\dot{\lambda}_2$  are distinct.

Proposition 1 leads directly to the following two corollaries regarding the boundedness of  $\Omega_{ij}$ .

Corollary 1: Whenever  $\lambda_i \to \lambda_j$  and  $\dot{\lambda}_i \not\to \dot{\lambda}_j$  then  $\Omega_{ij} \not\to \pm \infty$ .

*Proof:* If  $\Omega_{ij}$  would go to  $\pm \infty$  as  $\lambda_i \to \lambda_j$  in Eqs. (18) or (19), then it would be impossible for  $c_i$  and  $c_j$  to be continuous through the point where  $\lambda_i = \lambda_j$  which would contradict Proposition 1.

Corollary 2: Whenever  $\lambda_i \to \lambda_j$  and  $\dot{\lambda}_i \neq \dot{\lambda}_j$  then  $\mu_{ij} \to 0$ .

*Proof:* Since Eq. (17) must hold for all time and  $\Omega_{ij}$  must be bounded whenever  $\lambda_i \to \lambda_j$  and  $\dot{\lambda}_i \not\to \dot{\lambda}_j$ , then  $\mu_{ij}$  must go to zero.

From corollary 1 and 2 it is clear than any difficulties calculating  $\Omega_{ij}$  for repeated eigenvalues with distinct eigenvalue derivatives are purely numerical problems. Numerical simulations indicate that it is usually easy to calculate  $\Omega_{ij}$  in the neighborhood of two repeated eigenvalues as long as  $\dot{M}$  is not excessively large. In fact, Mills-Curran shows in Ref. 7 that at the instant where  $\lambda_i = \lambda_j$  and  $\dot{\lambda}_i \neq \dot{\lambda}_j$  a term analogous to  $\Omega_{ij}$  can be calculated using the distinct eigenvalue derivatives.

$$\Omega_{ij} = \frac{c_i^T \ddot{M} c_j}{2(\dot{\lambda}_i - \dot{\lambda}_i)} \tag{30}$$

However, this expression is not valid in the neighborhood of repeated eigenvalues. In a numerical simulation one usually does not have exact repeated eigenvalues. To avoid numerical problems of calculating the angular velocity terms in the neighborhood of repeated eigenvalues, the following approximation is introduced. Assume  $\Omega_{ij}$  is known at time step  $t_0$ . Then  $\Omega_{ij}$  at time step  $t_1 > t_o$  is approximated as

$$\Omega_{ij}(t_1) = \begin{cases}
\frac{\mu_{ij}}{\lambda_j - \lambda_i} & \text{for } |\lambda_i - \lambda_j| \ge \epsilon \\
\Omega_{ij}(t_0) + & \text{for } |\lambda_i - \lambda_j| < \epsilon \\
\dot{\Omega}_{ij}(t_0)(t_1 - t_0) & \text{for } |\lambda_i - \lambda_j| < \epsilon
\end{cases}$$
(3)

In other words, the  $\Omega_{ij}$  term is approximated linearly for as long as  $|\lambda_i - \lambda_j| < \epsilon$ . The derivative  $\Omega_{ij}(t_0)$  can be found numerically through a backwards difference method. For the present discussion we ignore the error in approximating  $\Omega_{ij}$ .

Proposition 2: Assume that  $|\lambda_i - \lambda_j| < \epsilon$  and that  $|\lambda_i - \lambda_j| \gg \epsilon$ , then the  $\Omega_{ij}$  approximation in Eq. (31) will introduce an error in M of the order of  $\epsilon^3$ .

*Proof:* Without loss of generality, let us assume that only the  $\lambda_1$  and  $\lambda_2$  are within  $\epsilon$  to being repeated eigenvalues.

$$\lambda_2 = \lambda_1 + \epsilon \tag{32}$$

Let M be the exact derivative obtained from the true  $[\Omega_{ij}]$  matrix and  $\underline{M}$  be the approximated derivative due to the approximated  $\underline{\Omega}_{ij}$  terms using Eq. (31). The error in M is given as

$$\Delta \dot{M} = \underline{\dot{M}}(\Lambda, C, [\underline{\Omega}]) - \dot{M}(\Lambda, C, [\Omega]) \tag{33}$$

After using Eqs. (7), (26) and (27)  $\Delta \dot{M}$  can be expressed as

$$\Delta \dot{M} = \epsilon \Delta \Omega_{12} (c_1 c_2^T + c_2 c_1^T) \tag{34}$$

The time span  $\Delta t = t_2 - t_1$  where  $|\lambda_1 - \lambda_2| < \epsilon$  can be estimated as follows. Let  $t_1$  be the time where the eigenvalue difference is less than  $\epsilon$  and  $t_2$  the time where the difference grows larger again than  $\epsilon$ . If it is assumed that  $|\dot{\lambda}_1 - \dot{\lambda}_2| \gg \epsilon$  than  $\lambda_1$  and  $\lambda_2$  can be assumed to be near linear between  $t_1$  and  $t_2$  as illustrated in Figure 1. The time  $\Delta t$  is approximately

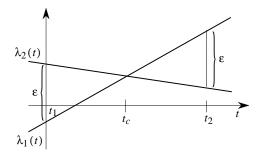


Fig. 1 Repeated Eigenvalue Illustration

related to the difference in eigenvalues  $\epsilon$  through

$$\Delta t \simeq \frac{2\epsilon}{\dot{\lambda}_1 - \dot{\lambda}_2} \tag{35}$$

During the interval  $[t_1, t_2]$ ,  $\underline{\Omega}_{12}$  is linearly extrapolated. Let us write the  $\Omega_{ij}$  term at time  $t_2$  as a

Taylor series expansion about time  $t_1$ .

$$\Omega_{ij}(t_2) = \Omega_{ij}|_{t_1} + \dot{\Omega}_{ij}|_{t_1} \Delta t 
+ \frac{1}{2!} \ddot{\Omega}_{ij}|_{t_1} \Delta t^2 + O(\Delta t^3)$$
(36)

The approximation  $\underline{\Omega}_{ij}$  is simply an first order truncation of Eq. (36).

$$\underline{\Omega}_{ij}(t_2) = \Omega_{ij}|_{t_1} + \dot{\Omega}_{ij}|_{t_1} \Delta t \tag{37}$$

Assuming that the third and higher order derivatives of  $\Omega_{12}$  are small compared to  $\Omega_{12}$ , the largest  $\Delta\Omega_{12}$  likely to be encountered would be of the order

$$\Delta\Omega_{12} \simeq \frac{1}{2}\ddot{\Omega}_{12}(t_1)\Delta t^2 + O(\Delta t^3)$$
 (38)

Using Eqs. (35) and (38),  $\Delta \dot{M}$  can be approximated as

$$\Delta \dot{M} \approx \frac{\epsilon^3 \ddot{\Omega}_{12}(t_1)}{(\dot{\lambda}_1 - \dot{\lambda}_2)^2} (c_1 c_2^T + c_2 c_1^T)$$
 (39)

which is of order  $\epsilon^3$ . If there are m pairs of eigenvalues within  $\epsilon$  of each other, then the total error in  $\Delta \dot{M}$  would be the sum of all m corresponding errors as shown in Eq. (39) and also be of order  $\epsilon^3$ .

Note that the approximation of  $\Omega_{ij}$  only directly affects M. The actual error in M in a numerical simulation would be related to the type of numerical integration used. The above analysis ignores the error implicit in approximating  $\dot{\Omega}_{ij}$ . If this approximation is not valid, then an error  $\Delta M$  would still be of order  $\epsilon^2$ . This error analysis will always break down whenever the corresponding eigenvalue derivatives loose their distinctiveness. This situation will be discussed in the following section.

#### B. Equal Eigenvalue Derivatives

The error  $\Delta M$  introduced through the approximation in Eq. (31) is more difficult to estimate whenever both  $\lambda_i = \lambda_j$  and  $\lambda_i = \lambda_j$ . However, it is possible to give a conservative error estimate for M.

Proposition 3: Let  $|\lambda_i - \lambda_j| \leq \epsilon$  and  $|\dot{\lambda}_i - \dot{\lambda}_j| \leq \epsilon$  during the time period  $[t_1, t_2]$ . Then at  $t_2$ , where the eigenvalues start to differ again by more than  $\epsilon$ , the error in M introduced by the approximation in Eq. (31) will be no more than of order  $\epsilon$ .

*Proof:* Without loss of generality, let's assume that only the first two eigenvectors are close, i.e.  $|\lambda_1 - \lambda_2| \leq \epsilon$ . The time period  $[t_1, t_2]$  spans the time where both eigenvalues and eigenvalue derivatives are almost equal. At worst the  $\lambda_1$  and  $\lambda_2$  would differ by  $\epsilon$ .

$$\lambda_2 = \lambda_1 + \epsilon \tag{40}$$

Eq. (25) can be written as

$$M = \lambda_1 E_{12} + \epsilon E_2 + \sum_{i=3}^n \lambda_i E_i \tag{41}$$

For this case the approximation in Eq. (31) only affects  $\Omega_{12}$ . Note that this  $\Omega_{12}$  term controls the rotational speed of the  $c_1$  and  $c_2$  eigenvectors in the plane spanned by the two. Eq. (41) shows that whenever there are nearly repeated eigenvalues, then the subspace spanned by the corresponding eigenvectors is important, not the individual eigenvectors themselves. Therefore approximating  $\Omega_{12}$  as in Eq. (31) will lead to an error in M of the order of  $\epsilon$  as long as  $|\lambda_1 - \lambda_2| < \epsilon$ .

Note that if the eigenvectors remain continuous during  $[t_1, t_2]$ , then no further modifications need be done after time  $t_2$ . However, whenever the eigenvalues and eigenvalue derivatives are equal it is possible for the eigenvectors to be discontinuous. Let the two integer sets  $R^-$  and  $R^+$  be defined as

$$R^{-} = \{1, 2, \dots, r\} \tag{42}$$

$$R^{+} = \{r+1, r+2, \dots, n\}$$
 (43)

Proposition 4: Let M be a continuous symmetric, positive definite matrix with a continuous derivative M. Assume M has r repeated eigenvalues which have equal derivatives. Then if  $c_i$   $(i \in R^-)$  is discontinuous then  $\Omega_{ip}$  is either discontinuous or zero for every  $p \in R^+$ .

Proof: Using Eqs. (7) and (26) we can express  $\dot{E}_i$  as

$$\dot{E}_i = -\sum_{i=1}^n \Omega_{ij} (c_j c_i^T + c_i c_j^T) \qquad i \neq j$$
 (44)

Without loss of generality, let the first r eigenvalues be repeated. Then  $E_{1-r}$  is defined as

$$E_{1-r} = E_1 + \ldots + E_r \tag{45}$$

Since the first r eigenvalues and their derivatives are equal, Eq. (27) can be written as

$$\dot{M} = \dot{\lambda}_1 E_{1-r} + \lambda_1 \dot{E}_{1-r} + \sum_{j=r+1}^{n} \dot{\lambda}_j E_j + \lambda_j \dot{E}_j$$
 (46)

Since M is continuous, the right hand side of the above equation also would have to be continuous whenever any eigenvectors were discontinuous. By definition the subspace  $E_{1-r}$  is invariant to any instantaneous change of base eigenvectors. However,

the terms  $\dot{E}_{1-r}$  and  $\dot{E}_{j}$  need further investigation. Using Eq. (44)  $\dot{E}_{1-r}$  can be reduced to

$$\dot{E}_{1-r} = -\sum_{i=1}^{r} \sum_{j=r+1}^{n} \Omega_{ij} (c_j c_i^T + c_i c_j^T)$$
 (47)

where the fact was used that  $\Omega_{ji} = -\Omega_{ij}$ . As expected, no  $\Omega_{ij}$  terms relating the eigenvectors of two repeated eigenvalues appear in  $\dot{E}_{1-r}$ .

The only possibility for  $\dot{E}_{1-r}$  to be invariant to any discontinuity in  $c_i$  ( $i \in R^-$ ) is for  $\Omega_{ip}$  to be either discontinuous or zero for every  $p \in R^+$ . Studying Eq. (44) the same can be said for  $\dot{E}_i$ .

Note that the eigenvector derivatives  $c_i$   $(i \in R^-)$  could be anything as long as  $\lambda_i = \lambda_j$  and  $\dot{\lambda}_i = \dot{\lambda}_j$   $(i,j \in R^-)$ . However, as soon as either the eigenvalues or their derivatives become distinct the corresponding eigenvectors and derivatives are uniquely determined again. If the eigenvectors are erroneously continuously forward integrated, then the corresponding C matrix would no longer diagonalize the current M(x) matrix. What is needed is a method to rotate the two eigenvectors within the plane spanned by them such that they once again diagonalize the mass matrix.

#### V. Stabilization using the Jacobi Method

No matter what method we use, and regardless of whether or not nearly repeated eigenvalues have been encountered, numerical integration errors degrade accuracy of the eigenvector matrix C. Without further adjustments the errors will accumulate and C will no longer properly diagonalize the current mass matrix M(x,t). These adjustments are particularly desirable during periods when the  $\Omega_{ij}$  terms are only being approximated and to handle cases of discontinuous eigenvectors.

We introduce a stabilization method base on the  $Jacobi\ method.^{12}$  The Jacobi method has been used for over a century because of its simplicity and stability. It finds the eigenvalues and eigenvectors of a symmetric matrix M by pre- and postmultiplying it by successive orthogonal rotation matrices  $P_i$  as is briefly outlined below.<sup>13</sup>

Let  $P_i$  be the *i*-th rotation matrix and  $\Lambda_k$  be the matrix obtained after pre- and postmultiplying M by the first  $k P_i$  matrices.

$$P_k^T \dots P_1^T P_0^T M P_0 P_1 \dots P_k = \Lambda_k \tag{48}$$

As  $k \to \infty$  the matrix  $\Lambda_k$  becomes diagonal with its entries being the eigenvalues of M. The eigenvector matrix C as defined in Eq. (1) is

$$C = P_k^T \dots P_1^T P_0^T \tag{49}$$

The orthogonal rotation matrix  $P_{k+1}$  is defined such that the i,j-th entry of  $\Lambda_k$  is zeroed. The matrix  $P_{k+1}$  is a diagonal matrix with the i-th and j-th diagonal elements being  $\cos\theta$ . The only two non-zero off-diagonal elements are the i,j-th element being  $-\sin\theta$  and the j,i-th element being  $\sin\theta$ . The rotation angle  $\theta$  is defined as

$$\theta = \frac{1}{2} \arctan \frac{2\Lambda_{ij}^k}{\Lambda_{ii}^k - \Lambda_{jj}^k}$$
 (50)

if the diagonal elements are distinct or as

$$\theta = \frac{\pi}{4} \tag{51}$$

if the diagonal elements are equal. Once the offdiagonal elements are small in magnitude, the the procedure is shown to have quadratic convergence.<sup>13</sup>

In the eigenfactor mass matrix parameterization method presented in this paper we already have a close approximation  $\hat{C}$  of the eigenvector matrix C.

$$\hat{C}M\hat{C}^T = \hat{\Lambda}_0 \tag{52}$$

Since the numerical integration is not perfect, or since some  $\Omega_{ij}$  terms are only being approximated, the  $\hat{\Lambda}_0$  matrix may not be exactly diagonal. To cancel the first off-diagonal element the rotation matrix  $P_1$  is constructed and operated on  $\hat{\Lambda}_0$ .

$$P_1^T \hat{\Lambda}_0 P_1 = \hat{\Lambda}_1 \tag{53}$$

This process is then repeated for each of the remaining off-diagonal elements. Assuming the matrix has k significant off-diagonal elements, the adjusted eigenvector matrix  $\hat{C}_{ad}$  becomes

$$\hat{C}_{ad} = P_k^T \dots P_1^T \hat{C} \tag{54}$$

Please note that each  $P_i\hat{C}$  update does not involve a full matrix multiplication. Actually only two eigenvectors are linearly combined (i.e. rotated) to form the new eigenvectors.

If no eigenvector discontinuity had occurred, then it was shown above that the error due to approximating  $\Omega_{ij}$  would be of the order of  $\epsilon^3$  for the case of distinct eigenvalue derivatives and at least of order  $\epsilon$  for the case of repeated eigenvalue derivatives. In either case the off-diagonal terms of  $\hat{\Lambda}_0$  would be very small to begin with. A Jacobi sweep refers to the process of sequentially zeroing each of the k off-diagonal elements. Since the Jacobi method has quadratic convergence and the off-diagonal terms are of order  $\epsilon^3$  or smaller to begin with, one Jacobi sweep will suffice to cancel any diagonalizing error of the C

matrix within machine accuracy for that particular integration step.

This Jacobi sweep should be used whenever two eigenvalues are near-equal and  $\Omega_{ij}$  terms are being approximated. Performing the approximations without the Jacobi sweeps was usually found to be stable for a single eigenvalue crossing. However, for repeated cases of near-equal eigenvalue events, the errors accumulate and drive the integration unstable in some simulations. Performing these Jacobi sweeps ensures that the current C and  $\Lambda$  matrices diagonalize the current mass matrix M(x) to a high degree of approximation and stabilizes the integration process.

For the case of repeated eigenvalues there is an infinite choice of eigenvectors that will diagonalize M. It was shown that for non-repeated eigenvalue derivatives there is a unique choice of eigenvectors that will generate the proper M matrix. The Jacobi method will only correct C such that it diagonalizes M without any regard to M. Therefore small residual state errors can still be expected even after the Jacobi sweep. However, numerical studies showed that the Jacobi sweeps dramatically improve the accuracy and the long term stability of the orthogonal square root eigenfactor parameterization.

If eigenvalues and their derivatives are equal, it was shown above that it is possible for the eigenvectors to be discontinuous. During the integration, discontinuous eigenvectors will cause rapidly growing off-diagonal terms of the  $\hat{\Lambda}_0$  matrix if no further action is taken. However, by performing a Jacobi sweep after each integration step where near-equal eigenvalues occur automatically rotates the two corresponding eigenvectors such that they again diagonalize the current M(x,t). Therefore discontinuous eigenvectors are handled with the same Jacobi sweep process used to ensure long-term stability.

During the periods where no eigenvalues are close to being equal (the common case), it is not necessary to perform a Jacobi sweep after each integration step. Numerical studies showed that performing it after each integration step caused a slightly larger long term error than simply performing it periodically due to an increased number of arithmetic operations.

#### VI. Results

A preliminary study of the orthogonal square root eigenfactor parameterization of a mass matrix was performed on the three-link system shown in Figure 2. The system was chosen to have a low number of degrees of freedom to simplify the analysis of the method. Also, since the system is conservative

the total system energy E remains constant and will provide a convenient way of measuring the current solution error.

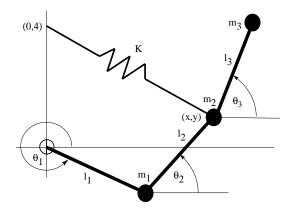


Fig. 2 Three-Link Manipulator System

All masses and rods were set to unit weight and length. The spring constant K was 0.2. The initial orientation angles are  $\theta_1 = -90^{\circ}$ ,  $\theta_2 = -30^{\circ}$  and  $\theta_3 = 0^{\circ}$ . The forward integration was performed with a variable step size Runge-Kutta method. The classic fourth-order Runge-Kutta method was the primary integrator which was compared to a thirdorder Runge-Kutta method if the difference in states between the two integration methods did not lie between two thresholds, then the integration step size got either scaled up or down. In all simulations run the high accuracy threshold was always set to  $1.510^{-2}$  times the low accuracy threshold. To compare two eigenvector matrices the Frobenius norm was used. To compare solutions based on two different integrations the average integration step size hwill be used. Assuming that the simulation involved n integration steps  $h_i$ , then  $\overline{h}$  is defined as

$$\overline{h} = \frac{1}{t_f} \sum_{i=0}^{n} h_i^2 \tag{55}$$

The norm of the total energy error is defined as

$$\|\Delta E\|_{L^{1}(0,t_{f};\Re)} = \frac{1}{t_{f}} \int_{0}^{t_{f}} |\Delta E| dt$$
 (56)

The resulting eigenvalues time evolution for up to 20 seconds is shown in Figure 3. For rigid multi-link system of order three or more no configuration was found that would make eigenvalues become exactly repeated. However, Figure 3 shows that  $\lambda_2$  and  $\lambda_3$  become very close at certain times. To track these rapid changes where  $\lambda_2 \approx \lambda_3$ , a variable step size integration method is essential. Every time these two eigenvalues become very close something interesting

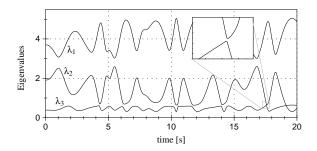


Fig. 3 Eigenvalue Time History

happens to corresponding eigenvectors. Away from a near eigenvalue encounter the eigenvectors oscillate normally as is seen in their angular velocity measures  $\Omega_{ij}$  in Figure 4. However, every close approach of  $\lambda_2$  and  $\lambda_3$  causes the corresponding eigenvector axes to "switch places." This switching is seen as a clear spike in the  $\Omega_{23}$  time history in Figure 4.

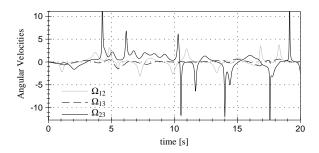


Fig. 4 Eigenvector Axis Angular Velocities

The following integration error studies were performed with  $\epsilon$  set small small enough such that  $\Omega_{ii}$ never invoked the linear approximation of Eq. (31). Just the standard  $\dot{S}$  and C equations are used. Case 1 is a simulation where no Jacobi sweeps are performed. This is essentially the same as using the method as proposed in Ref. 1. Case 2 is a simulation where a Jacobi sweep is performed after each integration step and in Case 3 the Jacobi sweep is performed only periodically after each 7th integration step. The time history of the total energy error for the first 100 seconds is shown in Figure 5. For each simulation the integration accuracy threshold was  $10^{-5}$  which resulted in an average step size of about  $\overline{h} = 0.04$  seconds. Without any Jacobi sweeps, the method clearly has a serious long term stability problem. The energy errors grows more erratic with time. Performing the Jacobi sweep after each integration step clearly smooths out the error curve. However, the arithmetic is starting to add an energy error of its own. Performing the Jacobi sweep only periodically after each seventh integration step was

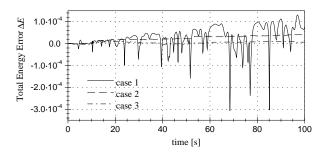


Fig. 5 Total Energy Error Evolutions

found to stabilize and minimize the total energy error. For this case, the errors end up being on the average about one order of magnitude smaller than for the other two cases. This general behavior was found to be true for all integration step sizes and other system configurations tested.

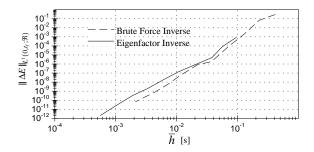


Fig. 6 Computational Accuracy Comparison

In Figure 6 the accuracy of the orthogonal square root eigenfactor mass matrix parameterization is compared to the accuracy obtained by performing the inverse  $M^{-1}$  directly. For the simple 3x3 system an exact matrix inverse formulation was used. For a given integration accuracy threshold the brute force inverse method had one to two orders of magnitude less accuracy. However, this was because the accuracy threshold enforced a larger average integration step size than for the new method. For a fairer comparison, Figure 6 compares the error norms relative to the average integration step size. Integrating the eigenfactors provides only a small decrease in accuracy compared to brute force inverse method. The brute force inverse method would be very difficult to beat for this low order dynamical system since it employs an exact matrix inverse. Taking the inverse for larger systems is known to be computationally very difficult and will inject significant arithmetic error on every time step. However, the integration of the eigenfactors is not expected to be more difficult for higher order systems. The major integration difficulties are already present in this low order system, since we have specifically addressed an example with frequent occurence of near-repeated eigenvalues. Therefore it is very encouraging to see the eigenfactor method integration error comparable to the exact brute force solution. For higher order systems the eigenfactor method is expected to provide better accuracy and stability. Parallelization of the present algorithm is easily accomplished and this is conjectured to be an extremly important computational feature for high-dimensional applications. However, at present time this has not yet been numerically verified and will be studied in future work.

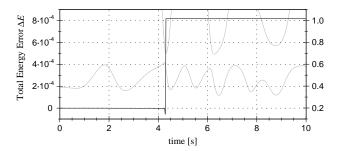


Fig. 7 Total Energy Error Evolution

To numerically study the integration accuracy of the  $\Omega_{ij}$  approximations in Eq. (31), the  $\epsilon$  term was set to 0.15. The integration accuracy threshold was set to  $10^{-5}$ . Between 4 and 5 seconds  $\lambda_2$  and  $\lambda_3$  are equal within this bound. The total energy norm for up to 10 seconds is shown in Figure 7. The eigenvalues  $\lambda_2$  and  $\lambda_3$  are plotted as a comparison in the background with their scale labeled on the right axis. As expected, even with the Jacobi sweeps being performed after any integration steps with  $\Omega_{ij}$  approximations, there is still a distinct jump in the total energy error when  $|\lambda_2 - \lambda_3| < \epsilon$ . For the case where the eigenvalues actually become equal and have distinct derivatives, a rough error estimate of  $\epsilon^3$  was predicted. Even though the eigenvalues never actually become equal in this situation, the error is still of the order of  $\epsilon^3$ . The system was also found to be stable for repeated cases of close eigenvalues, even with this crude  $\epsilon$  threshold. When no Jacobi sweeps were done and the  $\Omega_{ij}$  were only approximated as a constant as proposed in Ref. 1 then the solution was found to be unstable for the case of repeatetly close eigenvalues.

Note that the  $\epsilon$  used in Figure 7 is much larger than it would be normally used with this eigenfactor method. With double precision accuracy the difference between two eigenvalues can be become much smaller before any numerical difficulties occur. Since the linear approximation of  $\Omega_{ij}$  usually results in errors of the order of  $\epsilon^3$ , choosing  $\epsilon$  be to about  $1e^{-5}$ 

would suffice for most applications.

#### VII. Conclusion

An improved orthogonal square root eigenfactor parameterization of a symmetric, positive definite mass matrix has been presented. A key feature of this integration process proposed is the use of the Jacobi method to stabilize the solution for the eigenfactors. Repeated eigenvalues, repeated eigenvalue derivatives and discontinuous eigenvectors can be handled by this improved method as illustrated by an example. This method lends itself very well to a massively parallel computer implementation.

#### References

- Oshman, Y. and Bar-Itzhack, I. Y., "Eigenfactor Solution of the Matrix Riccati Equation A Continuous Square Root Algorithm," *IEEE Trans. on Automatic Control*, Vol. AC-30, No. 10, Oct. 1985, pp. 971–978.
- Kim, Y., Lee, S., and Junkins, J. L., "Eigenvector Derivatives for Mechanical Second - Order Systems," Journal of Guidance, Control and Dynamics, Vol. 18, No. 4, July-Aug. 1995, pp. 899-906.
- Lin, R. M. and Lim, M. K., "Eigenvector Derivatives of Structures with Rigid Body Modes," AIAA Journal, Vol. 34, No. 5, May 1996, pp. 1083-1085.
- Junkins, J. L. and Kim, Y., Introduction to Dynamics and Control of Flexible Structures. AIAA Education Series, Washington D.C., 1993.
- Schaub, H., Tsiotras, P., and Junkins, J. L., "Principal Rotation Representations of Proper NxN Orthogonal Matrices," International Journal of Engineering Science, Vol. 33, No. 15, Elsevier Science Ltd., Great Britain, 1995, pp. 2277-2295.
- Dailey, R. L., "Eigenvector Derivatives with Repeated Eigenvalues," AIAA Journal, Vol. 27, No. 4, April 1989, pp. 486-491.
- Mills-Curran, W. C., "Calculation of Eigenvector Derivatives for Structures with Repeated Eigenvalues," AIAA Journal, Vol. 26, No. 7, July 1988, pp. 867–871.
- Zhang, D.-W. and Wei, F.-S., "Computation of Eigenvector Derivatives with Repeated Eigenvalues Using a Complete Modal Space," AIAA Journal, Vol. 33, No. 9, May 1995, pp. 1749–1753.
- Zhang, Y.-Q. and Wang, W.-L., "Eigenvector Derivatives of Generalized Nondefective Eigenproblems With Repeated Eigenvalues," *Journal of Engineering for Gas Turbines and Power*, Vol. 117, Jan. 1995, pp. 207-112.
- Junkins, J. L. and Turner, J. D., Optimal Spacecraft Rotational Maneuvers. Elsevier Science Publishers, Netherlands, 1986.
- Bowen, R. M. and Wang, C.-C., Introduction to Vectors and Tensors, Vol. 1. Plenum Press, New York, 1976.
- Jacobi, C. G. J., "Über ein leichtes Verfahren die in der Theorie der Säculärstörungen vorkommenden Gleichungen numerisch aufzulösen," Crelle's Journal, Vol. 30, 1846, pp. 51-94.
- Bathe, K., Finite Element Procedures in Engineering Analysis. Prentice-Hall, Inc., New Jersey, 1982.